



THE EFFECT OF TEMPERATURE AND FLYWHEEL ON PERFORMANCE OF STIRLING ENGINE GAMMA TYPE

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1.0 INTRODUCTION

The Stirling engine is a theoretically working closed-cycle mechanical device with combustion in the Stirling cycle, or a modification thereof. This machine utilizes a compressed working fluid such as water, hydrogen, helium, nitrogen, or steam. This Stirling engine has higher efficiency with lower exhaust emissions than gasoline or diesel engines (1), (2), (3), .

The Stirling engine can be implemented and can be used as a distributed electric energy generator which is currently being looked at as renewable energy in overcoming global energy security and environmental impact (4). Solar thermal energy can be used to drive the piston in the stirling engine.

The Stirling engine works due to gas expansion when heated and followed by gas compression when cooled. The machine contains a quantity of gas that is moved between the cold and hot sides continuously. This gas transfer is possible due to the displacement piston which transfers the gas between the two sides and the power piston changes the internal volume due to the expansion and contraction of the gas. The moving piston is referred to as a regenerator which can regenerate air (5). The stirling engine is coupled to the generator shaft, the generator shaft will move when the engine piston moves, thus producing electricity. By utilizing solar heat to produce a temperature difference between the hot and cold parts of the stirling engine, we have obtained the mechanical energy from the stirling engine which is used to rotate the generator. The Stirling engine can be used to generate electricity that is environmentally friendly and of course cheaper because it does not require fuel (6).

In a thermodynamic review, it is known that the efficiency of the Stirling engine will increase as the operating temperature increases in the exoansion area. However, at the design level, this is limited by the ability of materials with high strength and thermal conductivity, as well as having a minimum coefficient of thermal expansion (7), (8).

This strling machine will become the object of further observation or research in order to obtain useful results for the future in terms of application, construction and efficiency. In this research, stirling engine design is designed with optimum stirling engine performance. The purpose of this study was to determine the optimum performance of the stirling engine in terms of power and torque by varying temperature. In this study, the Stirling engine was given a load at the Top Dead Point (TDC) of the piston power and saw the effect of this loading.

2.0 METHODOLOGY

2.1. Material

The designed stringing machine is a machine gamma (γ) type, with the following specifications :

No	Туре	Information	
1	Engine Type	Gamma (y)	
2	Phasa Angle	90 °	
3	Working Gas	Air	
4	Cooling	Water	
5	Heater	Solar Collector	

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The heat source comes from the stove. This variation aims to test the performance of the Stirling engine to the maximum and minimum levels.

2.2. Testing Procedures

Before conducting the test, the stove must be heated first, because the Stirling motor works with external combustion (9), in this case the stove used is a gas LPG as simulator to replace solar energy (10). In another study, burning spirit was used as a substitute for a source of heat energy (11). After the stove has been burning steadily, the fire is focused on the displacer cylinder (the hot part of the Stirling engine) to a predetermined temperature.

The use of the stove as a heat source is intended so that the input temperature can be regulated and stable.



Figure 1. Stirling Engine Parts

Caption :

- a. Flywheel
- b. Cold cylinder (Tc)
- c. Cooling water inlet
- d. Silinder piston displacer (TE)
- e. Bracket

- f. Lingkage piston displacer
- g. Cooling water outlet

The next procedure is to give the flywheel an initial rotation. After the stirling engine rotates, the parameters needed for performance analysis are recorded, namely, the air temperature in the hot cylinder (TE), the air temperature in the cold cylinder (TC) and the stirling engine speed (rpm). Then measure the engine speed using a tachometer. After all the data is obtained, the test is carried out five times in each specified temperature variation. In this variation the temperature maintained is 200°C, 300 °C, 400 °C, 500 °C, 600 °C and 700°C.

Performance testing is based on how much the rpm, power and torque that can be produced by the stirling engine with the parameters used are how big the temperature difference is between the hot and cold parts of the stirling engine.

3.0 RESULTS AND DISCUSSION

Stroke power piston, radius Crank power piston a. multiplied by two

• 0,025m x 2 = 0,05 m

b. Stroke displacer piston, radius Crank displacer dikali dua

• 0,04m x 2 = 0,08 m

Piston displeasure dimension

C.

• t = 0,1405 m

- d. Fluid chamber volume
 - Volme silinder power piston (VPP) VPP = π , r^2 , t

Volume siku penghubung (VSP)

$$VSP = P.L.T$$

- $= 3.5 \times 10^{-4} \text{ m}^{3}$
- Volume silinder displacer (VSD) . ν

$$SD = \pi \cdot r^2 \cdot t$$

 $= 21.37 \times 10^{-4} \text{m}^{3}$

3.1. Calculation of test results data before flywheel modification

Calculation of test results data before flywheel modification.

Table 1. test results data before flywheel modification

No	T _{and} (°C)	Tc (°C)	RPM
1	200	50	144
2	300	50	232
3	400	50	319
4	500	50	393
5	600	50	437
6	700	50	529

1. Calculation of the results of data collection

T_F = 200 °C = 473 K RPM = 144

Tc = 50 °C = 323 K

- The stroke volume when the piston is compressed (Vsc) and (Vs_{AND}):
- $V_{SC} = \pi r^2 x S = 3,14 x (0,026)^2 m x 0,054$ * $m = 1,14 \times 10^{-4} m^3$
- * $V_{SAND} = \pi r^2 x S = 3,14 x (0,055 m)^2 m x$ 0,08 m = 7,59 x 10 ⁻⁴ m³
- Compression ratio (r) : . Vsc + VtVsc + Vt
- r = Vt Vt٠ = = 5.38
- Temperature regenerator (T_R) • $\frac{\text{TE+TcTE+Tc}}{2} = \frac{473 \text{ K} + 323 \text{ K} 473 \text{ K} + 323 \text{ K}}{2}$
- * $T_R = 2$ 398 K
- Temperature Ratio (†) • ТсТс 323 К 323 К
- $t = \overline{tete} = 473 \text{ k} 473 \text{ k} = 0,68 \text{ K}$ *
- Step volume ratio (v) $1,14 \ge 10^{-4} \text{ m}^3$ $1,14 \ge 10^{-4} \text{ m}^3$ VscVsc $V = V_{VSEVSE} = 7,59 \times 10^{-4} \text{ m}^3 7,59 \times 10^{-4} \text{ m}^3 =$
- 0,15 m³ • Remaining volume ratio in cold cylinder ()

$$X_{DC}$$

$$X_{DC} = \frac{VDCVDC}{VSEVSE} = \frac{1.14 \times 10^{-4} \text{ m}^3 \text{ } 1.14 \times 10^{-4} \text{ } \text{m}^3}{7.59 \times 10^{-4} \text{ } \text{m}^3} =$$

$$V_{DC} = \frac{V_{SE}V_{SE}}{V_{SE}V_{SE}} = \frac{7.53 \times 10^{-4} \text{ m}^3 \text{ m}^{-1} \text{ m}^{-1$$

$$X_{OF} = VSEVSE = 7,59 \times 10^{-4} \text{ m}^3 7,59 \times 10^{-4} \text{ m}^3 = 0,499 \text{ m}^3$$

$$X_{\rm P} = \frac{VR}{VSEVSE} = \frac{1.31 \times 10^{-1}.31 \times 10^{-1}}{7.59 \times 10^{-4}7.59 \times 10^{-4}} = 0.17 \,\mathrm{m}$$

$X_R = v_{SEVSE} = 7,59 x 10^{-4}7,59 x 10^{-4} = 0,17 m^3$

Working Fluids in Stirling Engines

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The working fluid used in this stirling engine is air with a total air mass (m) which is entered into the stirling engine when room temperature and ambient (atmospheric) pressure. The following are the values for room temperature and air pressure used:

Room temperature (T_{like}) = 25° C = 302 K

Air pressure $(p_{air}) = 1$ atm

To calculate the total mass, the volume position must be in the maximum position. The maximum position of the gamma type stirling engine when the power piston is in the TDC position (Top Dead Point). Then the volume of the hot cylinder can be calculated as follows

IN_{AND} = (Volume silinder displacer) - (Volume piston Displacer)

= 21,37 x 10⁻⁴m³ - 11,02 x 10⁻⁴m³

 $= 10,35 \times 10^{-4} \text{m}^{-3}$

Vc = Cylinder Volume at TDC

 $= p r^{2} t$ = 3,14. (0,026 m)². 0,054 m

 $= 1.14 \times 10^{-4} \text{ m}^{3}$

Vsp = P.L.T

= 0,24 m . 0,074 m . 0,02 m
= 3,5 x
$$10^{-4}$$
 m³
= 10,35 x 10^{-4} m³ + 1,14 x 10^{-4} m³ + 3,5 x 10^{-4}
= 14,99 x 10^{-4} m³ \approx 0,001499 m³

For.

$$m = \frac{1.01325 \times 10^{5} Pa \times 0.001499 m3}{286 \frac{J}{Kg} K \times 302 K}$$

$$m = \frac{\frac{101325 N/m^2 x 0,001499 m}{286 \frac{Nm}{Kg} K x 302 K}}{286 \frac{Nm}{Kg} K x 302 K}$$

m = 0,00175 Kg

• Average pressure (Pmean)

Inside the Stirling engine cylinder there is a pressure that must be calculated both in compression and expansion conditions. To calculate the average pressure s used as follows:

 $\boldsymbol{P}_{\text{mean}} = \frac{2mRTc}{VsE\sqrt{S^2 - B^2}VsE\sqrt{S^2 - B^2}}$

Where the values of the coefficients a, S and B • $\alpha \alpha = tan^{-1} \frac{v \sin dx}{t + \cos dx - 1t + \cos dx - 1} = tan^{-1}$

 $0,68 + \cos 90^{\circ} - 10,68 + \cos 90^{\circ} - 1 = 25,07^{\circ}$

• S = t + 2t
$$X_{OF}$$
+ $\frac{4t Vr}{1+t} \frac{4t Vr}{1+t}$ + v + 2 X_{DC} + 1

• B=
$$\sqrt{t^2 + 2(t-1)v\cos dx + v^2 + 2t + 1}$$

= 1,68

for,

•
$$P_{mean} = \frac{2 \times 0.00175 kg \times 286 \frac{J}{kgK} \times 323 K}{7.59 \times 10^{-4} \text{ m}^3 \sqrt{(4.42)^2 - (1.68)^2}}$$

 $P_{mean} = 104230,49 \text{ m}^2 = 104230.49 \text{ Pa}$

Cycle Extreme Pressure

In the stirling engine there is also an extreme pressure that must be calculated. Extreme pressure is the maximum and minimum pressure that occurs in the Stirling cycle which is used as the driving energy of the Stirling engine.

Calculation of extreme pressure where the value of the coefficient c is as follows:

 $C = \frac{BB}{SS} = \frac{1,681,68}{4,424,42} = 0,38.$

• Maximum Pressure (P_{max})

The maximum pressure is the largest pressure value that occurs in the stirling engine which can be calculated as follows:

$$\frac{Pmax}{Pmean} = \sqrt{\frac{1+c}{1-c}Pmax} = \sqrt{\frac{1+c}{1-c}}$$

for,

for.

$$Pmax = \sqrt{\frac{1+0.38}{1-0.38}} \sqrt{\frac{1+0.38}{1-0.38}} \times 104230,49 \text{ Pa}$$
$$= 154261.12 \text{ Pa}$$

• Minimum Pressure (P_{min})

the minimum pressure on the stirling engine can also be calculated as follows:

$$\frac{Pmin}{Pmean} = \sqrt{\frac{1-c\ Pmin}{1+c\ Pmean}} = \sqrt{\frac{1-c}{1+c}}$$

$$Pmin = \sqrt{\frac{1-0.38}{1+0.38}} \sqrt{\frac{1-0.38}{1+0.38}} \times 104230,49 \text{ Pa}$$
$$= 73586.72 \text{ Pa}$$

• Stirling Engine Work Generated in One Cycle (Wi)

The work of one cycle is the difference between the incoming and outgoing calorific values or the sum of the work when the piston expands and compresses is.

 $We = W_{AND} + W_C$

Where are the values of Wc and W_{AND}will be equal to the number of calories so Qc = Wc, so does $W_{AND}\text{=}Q_{AND}$

• Expansion Work (W_{AND})

Expansion work is the work produced in process 3-4 in the ideal Stirling cycle. Expansion work (W_{AND}) is obtained as follows:

 $IN_{AND} = \frac{Pmean.VSE.\pi.c.sin\alpha Pmean.VSE.\pi.c.sin\alpha}{1 + \sqrt{1 - c^2}} = 20,83 \text{ J}$

Compression Work (Wc)

The compression work is the work given to process 1-2 in the ideal stirling cycle. The negative sign in the equation indicates that work is directed into the system.

$$|N_{\rm C} = - \frac{P \text{mean.VSE.}\pi.c.t.sin\alpha}{1 + \sqrt{1 - c^2}}$$

 $IN_{C} = -14,16 J$

• Stirling Engine Work (Wi)

So the stirling engine work per cycle is: Wi = 20,83 J - 14,16 J = 6,67 J

Which =
$$\frac{Wi \cdot nWi \cdot n}{60 \quad 60}$$

Which = $\frac{\frac{6.67 \text{ J} \times 1446.67 \text{ J} \times 144}{60 \quad 60}}{60}$ = 16,008 Watt





Figure 2. Graph of the Relationship between Temperature and RPM before modification



Figure 3. Graph of Relationship between Temperature and Power before modification



Torque (Nm)

Figure 4. Graph of the Relationship between Torque and Power before modification

3.2. Calculation of test results data after flywheel modification

On the flywheel, the Stirling engine is slightly modified to get optimal results. The modification made to the flywheel is to apply a load of 1 kg to the top dead center (TDC) of the power piston.





after doing the calculations from the data from the test results, the results obtained are as follows.



Figure 6. Graph of the Relationship between Temperature and RPM after modification



Figure 7. Graph of Relationship between Temperature and Power after modification



Figure 8. Graph of the Relationship between Torque and Power after modification

• Comparison before and after modification of the stirling engine flywheel



Figure 9. Comparison of RPM before and after modification

From the graph above, it can be seen that changes in the flywheel on the stirling engine affect the RPM. Changes to the flywheel help the stirling engine spin so that it gets bigger RPM results. Because the energy absorbed in the flywheel is flowed back to increase the flywheel rotation speed at the same input.



Temperature (°C)

Figure 10. Comparison of Power before and after modification

From the results of the modification of the flywheel on the stirling engine, it can be seen that there is an increase in the power produced. This is because the RPM on the stirling engine has increased.

4.0 CONCLUSION

From the implementation of the research and analysis of the data obtained, several conclusions can be drawn, namely:

- 1. At a test temperature of 200°C it produces a power of 16 Watts and a torque of 1.065 while at a test temperature of 700°C it produces a power of 105.27 Watts and a torque of 1.9012 Nm. So, the greater the temperature, the greater the power generated.
- 2. The increase in RPM due to flywheel modification on the Stirling engine is an average of 22.7%. The increase in RPM is due to the energy absorbed in the flywheel being flowed

back to increase the rotational speed of the flywheel at the same input.

3. The increase in power due to flywheel modification on the Stirling engine is an average of 22.7%.

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References

- Kongtragool B, Wongwises S. 2003. A review of solar-powered Stirling engines and low temperature differential Stirling engines. Renew Sustain Energy Rev.7(2):131–54.
- [2] Chen J, Yan Z, Chen L, Andresen B. 1998. Efficiency bound of a solar-driven Stirling heat engine system. Int J Energy Res. 22(9):805–12.
- [3] Topgül T, Okur M, Şahin F, Çınar C. Experimental investigation of the effects of hot-end and coldend connection on the performance of a gamma type Stirling engine. Eng Sci Technol an Int J. 2022;36.
- [4] Raghavendra H, Suryanarayana Raju P, Hemachandra Reddy K. Effect of Geometric and Operational Parameters on the Performance of a Beta-Type Stirling Engine: A Numerical Study. Iran J Sci Technol - Trans Mech Eng [Internet]. 2022;46(1). Available from: https://doi.org/10.1007/s40997-020-00406-0
- [5] Zare S, Tavakolpour-Saleh AR. Free piston Stirling engines: A review. Int J Energy Res. 2020;44(7):5039–70.
- [6] Singh UR, Kumar A. Review on solar Stirling engine: Development and performance. Therm Sci Eng Prog [Internet]. 2018;8(August):244–56. Available https://doi.org/10.1016/j.tsep.2018.08.016
- [7] Shendage DJ, Kedare SB, Bapat SL. Numerical investigations on the Dish–Stirling engine system. Int J Ambient Energy. 2019;40(3):274–84.
- [8] Asnaghi A, Ladjevardi SM, Saleh Izadkhast P, Kashani AH. Thermodynamics Performance Analysis of Solar Stirling Engines. ISRN Renew Energy. 2012;2012:1–14.
- [9] Sarkar J, Bhattacharyya S. Application of graphene and graphene-based materials in clean energy-related devices Minghui. Arch Thermodyn. 2012;33(4):23–40.

- [10] Khanjanpour MH, Rahnama M, Javadi AA, Akrami M, Tavakolpour-Saleh AR, Iranmanesh M. An experimental study of a gamma-type MTD stirling engine. Case Stud Therm Eng [Internet]. 2021;24(February):100871. Available from: https://doi.org/10.1016/j.csite.2021.100871
- [11] Joseph J, Mathew Louis E, Thomas B, Anurag K, Sankar V, Pullan TT. Fabrication and testing of a gamma type stirling engine. Mater Today Proc [Internet]. 2019;46:9641–5. Available from: https://doi.org/10.1016/j.matpr.2020.07.152